## organic compounds

Acta Crystallographica Section E **Structure Reports** Online

ISSN 1600-5368

## 5-Methyl-1,3-diphenyl-N-(5-phenyl-1,3,4-thiadiazol-2-yl)-1H-pyrazole-4carboxamide

## Chandra,<sup>a</sup> S. S. Mahesh,<sup>b</sup> N. Srikantamurthy,<sup>c</sup> K. B. Umesha,<sup>c</sup> K. Palani<sup>d</sup> and M. Mahendra<sup>a</sup>\*

<sup>a</sup>Department of Studies in Physics, Manasagangotri, University of Mysore, Mysore 570 006, India, <sup>b</sup>Department of Physics, Acharya Institute of Technology, Bangalore 560 090, India, <sup>c</sup>Department of Chemistry, Yuvaraja's College, University of Mysore, Mysore 570 005, India, and <sup>d</sup>SER-CAT, APS, Argonne National Laboratory, Argonne, II-60439 USA

Correspondence e-mail: mahendra@physics.uni-mysore.ac.in

Received 7 October 2013; accepted 20 October 2013

Key indicators: single-crystal X-ray study; T = 273 K; mean  $\sigma$ (C–C) = 0.004 Å; R factor = 0.049; wR factor = 0.133; data-to-parameter ratio = 13.4.

The asymmetric unit of the title compound  $C_{25}H_{10}N_5OS$ , contains two molecules, A and B. In molecule A, the dihedral angles between the pyrazole ring and the C-bound phenyl group, the N-bound phenyl group and the thiadiazole ring are 32.30(14), 52.25(14) and  $34.94(12)^{\circ}$ , respectively. The corresponding angles in molecule B are 33.32 (14), 50.67 (15), and 70.30 (12)°, respectively. In the crystal, the A and B molecules are linked by pairs of  $N-H \cdots N$  hydrogen bonds, generating  $R_2^2(8)$  loops. This dimer linkage is reinforced by two C-H···O hydrogen bonds and one C-H···N hydrogen bond.

#### **Related literature**

For the synthesis, see: Shridevi Doddaramappa et al. (2013). For a related structure, see: Chandra et al. (2012).



#### **Experimental**

#### Crystal data

$\gamma = 70.373 \ (2)^{\circ}$
V = 2220.4 (5) Å <sup>3</sup>
Z = 4
Mo $K\alpha$ radiation
$\mu = 0.17 \text{ mm}^{-1}$
T = 273  K
$0.30 \times 0.25 \times 0.20$ mm

#### Data collection

Bruker APEXII CCD area-detector	7768 independent reflections
diffractometer	5447 reflections with $I > 2\sigma(I)$
18748 measured reflections	$R_{\rm int} = 0.029$

### Refinement

$R[F^2 > 2\sigma(F^2)] = 0.049$	579 parameters
$wR(F^2) = 0.133$	H-atom parameters constrained
S = 1.02	$\Delta \rho_{\rm max} = 0.20 \ {\rm e} \ {\rm \AA}^{-3}$
7768 reflections	$\Delta \rho_{\rm min} = -0.19 \text{ e } \text{\AA}^{-3}$

#### Table 1 Hydrogen-bond geometry (Å, °).

$D - H \cdot \cdot \cdot A$	$D-\mathrm{H}$	$H \cdot \cdot \cdot A$	$D \cdots A$	$D - \mathbf{H} \cdot \cdot \cdot A$
N3−H21···N9 <i>B</i>	0.86	2.13	2.916 (3)	151
$N8B - H53 \cdots N4A$	0.86	2.07	2.902 (3)	163
$C4A - H6B \cdots O1A$	0.96	2.42	3.107 (3)	128
C29 <i>B</i> −H38 <i>C</i> ···N5 <i>A</i>	0.96	2.59	3.443 (3)	148
$C37B - H46 \cdots O2B$	0.93	2.41	3.184 (3)	141

Data collection: APEX2 (Bruker, 2009); cell refinement: SAINT (Bruker, 2009); data reduction: SAINT; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: PLATON (Spek, 2009); software used to prepare material for publication: SHELXL97.

Chandra would like to thank the University of Mysore for the award of an RFSMS fellowship under the head DV5/ Physics/389/RFSMS/2009-2010/10.07.2012.

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: HB7148).

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# supporting information

Acta Cryst. (2013). E69, o1736 [doi:10.1107/S1600536813028766]

# 5-Methyl-1,3-diphenyl-*N*-(5-phenyl-1,3,4-thiadiazol-2-yl)-1*H*-pyrazole-4carboxamide

## Chandra, S. S. Mahesh, N. Srikantamurthy, K. B. Umesha, K. Palani and M. Mahendra

## S1. Comment

As part of our ongoing studies of pyrazole derivatives (Shridevi Doddaramappa, *et al.*, 2013), the title compound, (I), was prepared and characterized by single-crystal X-ray diffraction. It shows potential anticancer activity against the aurora kinase enzyme: the full results will be reported elsewhere.

In the molecular structure of the title compound (Fig. 1), two molecules (A and B) present in an asymmetric unit have heterocyclic ring moleties exhibiting planar conformation, with their maximum deviations found on ring planes from N1A and C19A are 0.011 (2) Å and 0.005 (2) Å, respectively. The bond lengths are comparable to a related structure (Chandra *et al.*, 2012).

In the molecules A and B, pyrazole moiety makes a dihedral angle of 34.94 (12)°, 76.83 (12)°, 50.67 (13)° and 33.32 (14)° with the phenyl rings (C5A–C10A, C11A–C16A and C30B–C35B, C36B–C41B), respectively. Thiadiazole moiety makes a dihedral angle of 58.01 (13)°, 68.82 (13)°, 79.35 (13)° and 70.30 (12)° with pyrazole and benzene rings, for A and B, respectively.

The crystal structure features C—H···N and C—H···O hydrogen bonds. The packing diagram of the molecules exhibit dimers with stacking feature when viewed down the c axis is shown in Fig. 2.

## **S2. Experimental**

A solution of pyrazole-4-carboxylic acid (1 mmol) in dry dichloromethane (5 ml) was cooled to  $0^{\circ}$  C and added ethyl-(*N'*,*N'*-dimethylamino)propylcarbodiimide hydrochloride (EDC·HCl, 1.2 mmol) and HOBt (1.2 mmol). To this reaction mixture 2-amino-5-phenyl-1,3,4- thiadiazole (1 mmol) was added and stirred at room temperature for 6–8 h. After completion of the reaction, the reaction mixture was extracted with ethyl acetate (2 × 25 ml) and the combined organic phase was washed with brine, dried over anhydrous sodium sulfate. Ethyl acetate was distilled off and the residue thus obtained was purified by recrystallization in EtOH to get the title compound as colourless blocks.

## **S3. Refinement**

H atoms were placed at idealized positions and allowed to ride on their parent atoms with N–H distance is equal to 0.86 Å and C–H distances in the range of 0.93 to 0.96 Å;  $U_{iso}(H) = 1.2-1.5U_{eq}(\text{carrier atom})$  for all H atoms.



## Figure 1

Perspective diagram of (I) with 50% probability displacement ellipsoids.



## Figure 2

Packing diagram of the molecule viewed down the 'c' axis.

## 5-Methyl-1,3-diphenyl-N-(5-phenyl-1,3,4-thiadiazol-2-yl)-1H-pyrazole-4-carboxamide

Z = 4

F(000) = 912

 $\theta = 1.7 - 25.0^{\circ}$ 

 $\mu = 0.17 \text{ mm}^{-1}$ 

Block, colourless

 $0.30 \times 0.25 \times 0.20$  mm

T = 273 K

 $D_{\rm x} = 1.309 {\rm Mg m^{-3}}$ 

Mo *K* $\alpha$  radiation,  $\lambda = 0.71073$  Å

Cell parameters from 7768 reflections

#### Crystal data

 $\begin{array}{l} C_{25}H_{19}N_5OS\\ M_r = 437.52\\ Triclinic, P\overline{1}\\ Hall symbol: -P 1\\ a = 10.7039 (14) Å\\ b = 12.9341 (17) Å\\ c = 17.478 (2) Å\\ a = 77.343 (2)^{\circ}\\ \beta = 82.865 (2)^{\circ}\\ \gamma = 70.373 (2)^{\circ}\\ V = 2220.4 (5) Å^3 \end{array}$ 

### Data collection

Bruker APEXII CCD area-detector	$R_{\rm int} = 0.029$
diffractometer	$\theta_{\rm max} = 25.0^{\circ}, \ \theta_{\rm min} = 1.7^{\circ}$
$\omega$ and $\varphi$ scans	$h = -12 \rightarrow 12$
18748 measured reflections	$k = -15 \rightarrow 15$
7768 independent reflections	$l = -20 \longrightarrow 20$
5447 reflections with $I > 2\sigma(I)$	

#### Refinement

Refinement on $F^2$	Secondary atom site location: difference Fourier
Least-squares matrix: full	map
$R[F^2 > 2\sigma(F^2)] = 0.049$	Hydrogen site location: inferred from
$wR(F^2) = 0.133$	neighbouring sites
S = 1.02	H-atom parameters constrained
7768 reflections	$w = 1/[\sigma^2(F_o^2) + (0.0689P)^2]$
579 parameters	where $P = (F_o^2 + 2F_c^2)/3$
0 restraints	$(\Delta/\sigma)_{\rm max} < 0.001$
Primary atom site location: structure-invariant	$\Delta \rho_{\rm max} = 0.20 \text{ e } \text{\AA}^{-3}$
direct methods	$\Delta \rho_{\rm min} = -0.19 \text{ e } \text{\AA}^{-3}$

### Special details

**Geometry**. Bond distances, angles *etc*. have been calculated using the rounded fractional coordinates. All su's are estimated from the variances of the (full) variance-covariance matrix. The cell e.s.d.'s are taken into account in the estimation of distances, angles and torsion angles

**Refinement**. Refinement on  $F^2$  for ALL reflections except those flagged by the user for potential systematic errors. Weighted *R*-factors *wR* and all goodnesses of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The observed criterion of  $F^2 > \sigma(F^2)$  is used only for calculating *-R*-factor-obs *etc*. and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*-factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(Å^2)$ 

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	
S1A	0.77966 (6)	0.57443 (5)	0.11413 (3)	0.0486 (2)	
O1A	0.52592 (17)	0.57319 (15)	0.14214 (10)	0.0696 (7)	
N1A	0.24119 (19)	0.51919 (16)	0.32617 (11)	0.0509 (7)	
N2A	0.3029 (2)	0.40699 (16)	0.34827 (11)	0.0528 (7)	
N3	0.66483 (18)	0.44976 (15)	0.23031 (10)	0.0459 (7)	

N4A	0.89440 (19)	0.40837 (15)	0.21844 (10)	0.0479 (7)
N5A	0.99500 (19)	0.44439 (16)	0.17621 (11)	0.0491 (7)
C1A	0.4177 (2)	0.38576 (19)	0.30667 (13)	0.0470 (8)
C2A	0.4297 (2)	0.48482 (19)	0.25603 (13)	0.0471 (8)
C3A	0.3132 (2)	0.5683 (2)	0.26966 (13)	0.0503 (8)
C4A	0.2660 (3)	0.6889 (2)	0.23304 (15)	0.0661 (10)
C5A	0.1144 (2)	0.5672 (2)	0.36390 (13)	0.0520 (9)
C6A	0.0175 (3)	0.5179 (2)	0.36746 (15)	0.0643 (10)
C7A	-0.1019(3)	0.5587 (3)	0.40836 (18)	0.0775 (11)
C8A	-0.1239(3)	0.6480(3)	0.44329 (18)	0.0830(14)
C9A	-0.0278(3)	0.6974(3)	0.43862(17)	0.0030(11) 0.0834(12)
C10A	0.0270(3)	0.6563(2)	0.39990 (16)	0.0691 (11)
	0.0923(3)	0.0505(2)	0.31/28(14)	0.0071(11)
C12A	0.5030(2) 0.5017(3)	0.20913(19) 0.1040(2)	0.31420(14) 0.38506(15)	0.0474(8)
C12A	0.5017(3)	0.1949(2) 0.0835(2)	0.38500(15) 0.20154(18)	0.0385(10)
CIAA	0.5750(3)	0.0855(2)	0.39134(10)	0.0743(11)
CI4A CI5A	0.04/3(3)	0.0437(3)	0.3283(2)	0.0820 (13)
CI5A	0.6500 (3)	0.1148 (2)	0.25814 (19)	0.0734 (12)
CI6A	0.5786(2)	0.2267 (2)	0.25111 (15)	0.0580 (9)
CI/A	0.5401 (2)	0.5061 (2)	0.20410 (14)	0.0495 (8)
C18A	0.7777 (2)	0.46898 (18)	0.19296 (12)	0.0417 (7)
C19A	0.9504 (2)	0.53004 (18)	0.12061 (13)	0.0438 (8)
C20A	1.0379 (2)	0.58313 (18)	0.06721 (12)	0.0440 (8)
C21A	1.1676 (3)	0.5616 (2)	0.08475 (15)	0.0591 (9)
C22A	1.2503 (3)	0.6097 (2)	0.03406 (16)	0.0716 (11)
C23A	1.2041 (3)	0.6815 (2)	-0.03456 (16)	0.0662 (11)
C24A	1.0754 (3)	0.7045 (2)	-0.05280 (14)	0.0587 (10)
C25A	0.9926 (3)	0.65537 (19)	-0.00233 (13)	0.0532 (8)
S2B	0.81627 (7)	0.14175 (5)	0.48058 (3)	0.0537 (2)
O2B	0.98933 (19)	0.01874 (14)	0.37824 (9)	0.0678 (7)
N6B	1.2354 (2)	0.11455 (16)	0.16431 (11)	0.0509 (7)
N7B	1.1838 (2)	0.04476 (16)	0.14004 (11)	0.0523 (7)
N8B	0.91824 (19)	0.20392 (15)	0.33307 (10)	0.0487 (7)
N9B	0.7403 (2)	0.33063 (16)	0.38824 (10)	0.0525 (7)
N10B	0.6575 (2)	0.34209 (16)	0.45472 (11)	0.0539(7)
C26B	1.0909 (2)	0.02892 (18)	0.19482 (13)	0.0458 (8)
C27B	1.0831 (2)	0.08937 (18)	0.25492 (12)	0.0447 (8)
C28B	1.1771 (2)	0.14337 (19)	0.23367 (13)	0.0482 (8)
C29B	1.2217 (3)	0.2113 (2)	0.27610 (15)	0.0650 (10)
C30B	1.3427 (3)	0.1439 (2)	0.11818 (14)	0.0557 (9)
C31B	1.4489 (3)	0.0614 (3)	0.09391 (16)	0.0724 (11)
C32B	1 5488 (3)	0.0908(3)	0.04525 (18)	0.0907(14)
C33B	1 5409 (4)	0.0000(3)	0.02129(18)	0.0925 (16)
C34B	1.4365 (4)	0.2816 (3)	0.04664(18)	0.0860(16)
C35B	1 3356 (3)	0.2547(2)	0.09550 (16)	0.0695 (11)
C36B	1.0000(0)	-0.03876(18)	0.09330(10) 0.18330(14)	0.0093(11)
C37P	0.0612(2)	-0.10363(10)	0.10330(17) 0.24401(15)	0.0401(0)
C38P	0.9012(3)	-0.1677(2)	0.24471(13) 0.23070(18)	0.0303 (9)
C30D	0.0073(3)	-0.1672(2)	0.23079(10) 0.1564(2)	0.0000(11)
CJYD	0.0040(3)	-0.1072 (2)	0.1304 (2)	0.0827(12)

C40B	0.9107 (4)	-0.1026 (3)	0.09536 (19)	0.1041 (18)
C41B	0.9826 (3)	-0.0384 (3)	0.10839 (16)	0.0852 (13)
C42B	0.9947 (2)	0.09754 (19)	0.32675 (13)	0.0474 (8)
C43B	0.8266 (2)	0.23077 (19)	0.39388 (12)	0.0450 (8)
C44B	0.6846 (2)	0.25151 (19)	0.50738 (13)	0.0484 (8)
C45B	0.6065 (3)	0.2402 (2)	0.58222 (13)	0.0524 (9)
C46B	0.6323 (3)	0.1389 (2)	0.63370 (15)	0.0765 (11)
C47B	0.5571 (4)	0.1274 (3)	0.70274 (17)	0.0940 (14)
C48B	0.4564 (3)	0.2173 (3)	0.72158 (17)	0.0841 (13)
C49B	0.4298 (3)	0.3172 (3)	0.67167 (17)	0.0773 (11)
C50B	0.5042 (3)	0.3306 (2)	0.60176 (15)	0.0676 (11)
H6A	0.17840	0.70790	0.21520	0.0990*
H6B	0.32520	0.70370	0.18920	0.0990*
H6C	0.26380	0.73310	0.27100	0.0990*
H8	0.03230	0.45780	0.34260	0.0770*
H9	-0.16740	0.52520	0.41200	0.0930*
H10	-0.20460	0.67550	0.47050	0.1000*
H11	-0.04420	0.75920	0.46180	0.1000*
H12	0.15870	0.68860	0.39810	0.0830*
H14	0.45160	0.22100	0.42840	0.0700*
H15	0.57220	0.03490	0.43930	0.0890*
H16	0.69560	-0.03180	0.33340	0.0980*
H17	0.70010	0.08760	0.21510	0.0880*
H18	0.58100	0.27460	0.20320	0.0700*
H21	0.67280	0.39960	0.27240	0.0550*
H28	1.19930	0.51400	0.13130	0.0710*
H29	1.33780	0.59380	0.04620	0.0860*
H30	1.26010	0.71440	-0.06850	0.0790*
H31	1.04400	0.75300	-0.09910	0.0700*
H32	0.90560	0.67080	-0.01500	0.0640*
H38A	1.31680	0.19090	0.27100	0.0970*
H38B	1.19340	0.19780	0.33060	0.0970*
H38C	1.18360	0.28920	0.25410	0.0970*
H40	1.45380	-0.01330	0.10990	0.0870*
H41	1.62190	0.03540	0.02880	0.1090*
H42	1.60730	0.21950	-0.01250	0.1110*
H43	1.43280	0.35600	0.03100	0.1030*
H44	1.26400	0.31040	0.11280	0.0840*
H46	0.97670	-0.10430	0.29620	0.0680*
H47	0.85770	-0.21180	0.27280	0.0820*
H48	0.81530	-0.21050	0.14750	0.0990*
H49	0.89380	-0.10180	0.04430	0.1250*
H50	1.01310	0.00590	0.06590	0.1020*
H53	0.92810	0.25770	0.29660	0.0580*
H60	0.70160	0.07760	0.62150	0.0920*
H61	0.57490	0.05850	0.73660	0.1130*
H62	0.40610	0.21000	0.76860	0.1010*
H63	0.36030	0.37790	0.68460	0.0930*

# supporting information

H64	0.48530	0.39	990	0.56820	0.0810*	
Atomic displacement parameters $(Å^2)$						
	$U^{11}$	U <sup>22</sup>	$U^{33}$	$U^{12}$	$U^{13}$	$U^{23}$
S1A	0.0405 (4)	0.0475 (3)	0.0524 (4)	-0.0139 (3)	-0.0025 (3)	0.0014 (3)
O1A	0.0463 (11)	0.0901 (13)	0.0533 (10)	-0.0160 (10)	-0.0047 (8)	0.0176 (10)
N1A	0.0368 (12)	0.0560 (12)	0.0572 (12)	-0.0135 (10)	0.0044 (10)	-0.0114 (10)
N2A	0.0436 (13)	0.0564 (13)	0.0590 (12)	-0.0181 (10)	0.0026 (10)	-0.0117 (10)
N3	0.0370 (12)	0.0490 (11)	0.0457 (11)	-0.0141 (9)	-0.0006 (9)	0.0031 (9)
N4A	0.0367 (12)	0.0549 (12)	0.0480 (11)	-0.0161 (10)	0.0002 (9)	-0.0001 (9)
N5A	0.0383 (12)	0.0568 (12)	0.0491 (11)	-0.0169 (10)	-0.0009 (9)	-0.0019 (9)
C1A	0.0371 (14)	0.0562 (15)	0.0488 (13)	-0.0160 (12)	0.0014 (11)	-0.0127 (11)
C2A	0.0359 (14)	0.0560 (14)	0.0469 (13)	-0.0129 (12)	-0.0020 (11)	-0.0073 (11)
C3A	0.0382 (15)	0.0602 (15)	0.0510 (14)	-0.0165 (13)	0.0003 (11)	-0.0078 (12)
C4A	0.0471 (17)	0.0640 (17)	0.0733 (17)	-0.0092(13)	0.0051 (13)	-0.0028(14)
C5A	0.0379 (15)	0.0636 (16)	0.0512 (14)	-0.0147 (13)	0.0033 (11)	-0.0098(12)
C6A	0.0460 (17)	0.0695 (17)	0.0750 (18)	-0.0179 (14)	0.0012 (14)	-0.0122(14)
C7A	0.0440 (18)	0.088 (2)	0.091 (2)	-0.0201 (16)	0.0068 (16)	-0.0051 (18)
C8A	0.052 (2)	0.102 (3)	0.078 (2)	-0.0100 (19)	0.0187 (16)	-0.0174 (19)
C9A	0.073 (2)	0.096 (2)	0.080 (2)	-0.0194 (19)	0.0174 (18)	-0.0381(18)
C10A	0.0551 (19)	0.086(2)	0.0730 (18)	-0.0249(16)	0.0054 (15)	-0.0305(16)
C11A	0.0368 (14)	0.0545(14)	0.0565 (14)	-0.0194(12)	-0.0008(11)	-0.0151(12)
C12A	0.0505 (17)	0.0624 (17)	0.0636 (16)	-0.0209(14)	0.0003 (13)	-0.0111(13)
C13A	0.070 (2)	0.0608 (18)	0.085 (2)	-0.0195(16)	-0.0054(17)	0.0006 (16)
C14A	0.068(2)	0.0597(18)	0.113(3)	-0.0102(16)	0.000 (2)	-0.0242(19)
C15A	0.063(2)	0.073 (2)	0.087(2)	-0.0178(16)	0.0095 (16)	-0.0350(17)
C16A	0.0479(16)	0.0666(17)	0.0635(16)	-0.0202(14)	0.0009 (13)	-0.0197(13)
C17A	0.0414(15)	0.0566(14)	0.0475 (14)	-0.0156(12)	-0.0015(11)	-0.0040(12)
C18A	0.0385(14)	0.0443(12)	0.0424(12)	-0.0143(11)	0.0008 (10)	-0.0083(10)
C19A	0.0433(14)	0.0446(13)	0.0457(13)	-0.0168(11)	-0.0011(11)	-0.0094(11)
C20A	0.0438 (15)	0.0434 (12)	0.0496 (13)	-0.0196(11)	0.0011 (11)	-0.0117(10)
C21A	0.0543(17)	0.0670(16)	0.0601 (16)	-0.0306(14)	-0.0089(13)	0.0003(13)
C22A	0.0560(19)	0.091 (2)	0.0782(19)	-0.0424(17)	-0.0053(15)	-0.0063(16)
C23A	0.069 (2)	0.0742 (18)	0.0649 (17)	-0.0431(16)	0.0078 (15)	-0.0071(14)
C24A	0.069(2)	0.0554 (15)	0.0523 (15)	-0.0265(14)	-0.0017(13)	-0.0018(12)
C25A	0.0500(16)	0.0549(14)	0.0536(14)	-0.0189(13)	-0.0047(12)	-0.0034(12)
S2B	0.0580 (4)	0.0537(4)	0.0400 (3)	-0.0105(3)	-0.0003(3)	-0.0026(3)
02B	0.0840(14)	0.0523(10)	0.0497(10)	-0.0100(10)	0.0055 (9)	0.0026 (8)
N6B	0.0495(13)	0.0572(12)	0.0518(12)	-0.0250(11)	0.0016 (10)	-0.0118(10)
N7B	0.0555(14)	0.0553(12)	0.0515(12)	-0.0261(11)	0.0042(10)	-0.0120(10)
N8B	0.0518 (13)	0.0473 (11)	0.0406 (10)	-0.0137(10)	0.0008 (9)	-0.0002(9)
N9B	0.0555(14)	0.0518 (12)	0.0420 (11)	-0.0106(11)	0.0018 (10)	-0.0047(9)
N10B	0.0561 (14)	0.0562(12)	0.0444 (11)	-0.0126(11)	0.0021 (10)	-0.0105(10)
C26B	0.0481(15)	0.0430(12)	0.0449(13)	-0.0149(11)	-0.0002(11)	-0.0063(10)
C27B	0.0438(15)	0.0433(12)	0.0425(12)	-0.0098(11)	-0.0035(11)	-0.0046(10)
C28B	0.0430(15)	0.0532(12)	0.0471(13)	-0.0141(12)	-0.0035(11)	-0.0078(11)
C29B	0.0605 (18)	0.0777 (18)	0.0663 (17)	-0.0273(15)	-0.0106(14)	-0.0209(14)

C30B	0.0530 (17)	0.0725 (18)	0.0487 (14)	-0.0323 (15)	-0.0037 (12)	-0.0058 (13)
C31B	0.070 (2)	0.085 (2)	0.0674 (18)	-0.0339 (18)	0.0174 (15)	-0.0222 (16)
C32B	0.073 (2)	0.131 (3)	0.083 (2)	-0.050 (2)	0.0238 (18)	-0.039 (2)
C33B	0.094 (3)	0.140 (3)	0.072 (2)	-0.082 (3)	0.0101 (19)	-0.016 (2)
C34B	0.094 (3)	0.103 (3)	0.077 (2)	-0.065 (2)	-0.012 (2)	0.0075 (19)
C35B	0.065 (2)	0.0750 (19)	0.0731 (18)	-0.0354 (16)	-0.0157 (15)	0.0036 (15)
C36B	0.0483 (15)	0.0417 (13)	0.0556 (14)	-0.0168 (11)	0.0073 (12)	-0.0134 (11)
C37B	0.0570 (17)	0.0470 (14)	0.0613 (15)	-0.0164 (13)	0.0075 (13)	-0.0082 (12)
C38B	0.0621 (19)	0.0520 (16)	0.091 (2)	-0.0262 (14)	0.0218 (16)	-0.0141 (15)
C39B	0.092 (2)	0.081 (2)	0.102 (2)	-0.0551 (19)	0.029 (2)	-0.0482 (19)
C40B	0.148 (4)	0.136 (3)	0.076 (2)	-0.100 (3)	0.022 (2)	-0.047 (2)
C41B	0.127 (3)	0.106 (2)	0.0583 (17)	-0.085 (2)	0.0142 (17)	-0.0237 (16)
C42B	0.0473 (15)	0.0507 (14)	0.0413 (13)	-0.0129 (12)	-0.0072 (11)	-0.0043 (11)
C43B	0.0450 (15)	0.0500 (14)	0.0387 (12)	-0.0142 (12)	-0.0022 (11)	-0.0073 (10)
C44B	0.0515 (16)	0.0536 (14)	0.0397 (12)	-0.0157 (12)	-0.0042 (11)	-0.0090 (11)
C45B	0.0513 (16)	0.0632 (16)	0.0434 (13)	-0.0184 (13)	-0.0024 (12)	-0.0116 (12)
C46B	0.081 (2)	0.0732 (19)	0.0565 (17)	-0.0116 (17)	0.0165 (15)	-0.0057 (14)
C47B	0.100 (3)	0.097 (2)	0.0641 (19)	-0.025 (2)	0.0201 (19)	0.0038 (17)
C48B	0.071 (2)	0.123 (3)	0.0550 (17)	-0.034 (2)	0.0165 (16)	-0.0164 (19)
C49B	0.057 (2)	0.103 (2)	0.0642 (18)	-0.0075 (18)	0.0030 (15)	-0.0323 (18)
C50B	0.065 (2)	0.0756 (19)	0.0543 (16)	-0.0101 (16)	-0.0016 (14)	-0.0168 (14)

## Geometric parameters (Å, °)

S1A—C18A	1.717 (2)	C8A—H10	0.9300
S1A-C19A	1.732 (2)	C9A—H11	0.9300
S2B—C43B	1.707 (2)	C10A—H12	0.9300
S2B—C44B	1.733 (2)	C12A—H14	0.9300
01AC17A	1.220 (3)	C13A—H15	0.9300
O2B—C42B	1.215 (3)	C14A—H16	0.9300
N1A—C5A	1.433 (3)	C15A—H17	0.9300
N1A—N2A	1.366 (3)	C16A—H18	0.9300
N1A—C3A	1.356 (3)	C21A—H28	0.9300
N2A—C1A	1.324 (3)	C22A—H29	0.9300
N3—C17A	1.370 (3)	C23A—H30	0.9300
N3—C18A	1.372 (3)	C24A—H31	0.9300
N4A—C18A	1.304 (3)	C25A—H32	0.9300
N4A—N5A	1.382 (3)	C26B—C27B	1.420 (3)
N5A—C19A	1.299 (3)	C26B—C36B	1.478 (3)
N3—H21	0.8600	C27B—C42B	1.476 (3)
N6B—C28B	1.361 (3)	C27B—C28B	1.380 (3)
N6B—N7B	1.364 (3)	C28B—C29B	1.485 (4)
N6B-C30B	1.429 (4)	C30B—C31B	1.369 (4)
N7B—C26B	1.327 (3)	C30B—C35B	1.379 (4)
N8B—C42B	1.365 (3)	C31B—C32B	1.385 (5)
N8B—C43B	1.373 (3)	C32B—C33B	1.364 (6)
N9B—C43B	1.303 (3)	C33B—C34B	1.357 (6)
N9B—N10B	1.374 (3)	C34B—C35B	1.382 (5)

N10B—C44B	1.292 (3)	C36B—C41B	1.376 (4)
N8B—H53	0.8600	C36B—C37B	1.377 (4)
C1A—C2A	1.424 (3)	C37B—C38B	1.380 (4)
C1A—C11A	1.464 (3)	C38B—C39B	1.359 (5)
$C^2A$ — $C^{17A}$	1.462 (3)	C39B—C40B	1.359(5)
$C_2A = C_3A$	1.102(3) 1.383(3)	C40B-C41B	1.375(5)
$C_{3A}$ $C_{4A}$	1.303(3) 1 487(3)	C44B-C45B	1.375(3) 1.469(3)
$C_{5A}$ $C_{6A}$	1.407(5) 1 377(4)	C45B C50B	1.409(3) 1.380(4)
$C_{5A} = C_{10A}$	1.377(4)	C45B C46B	1.300(4) 1.380(2)
C6A C7A	1.371(4) 1.381(5)	$C_{45B} = C_{45B}$	1.300(3) 1.374(4)
C7A C8A	1.361(5)	C47B $C48B$	1.37 + (+) 1.364 (5)
$C^{A}$	1.301(5)	$C_{47}B_{}C_{48}B_{}C_{4$	1.304(3) 1.254(5)
C0A = C10A	1.308(3) 1.271(5)	C40D = C50D	1.334(3) 1.284(4)
CIIA CI2A	1.3/1(3) 1.202(2)	$C_{49} = C_{50} = C_{50}$	1.364 (4)
CIIA—CIZA	1.392(3)	C29D—H38A	0.9000
	1.380(3)	C29B—H38B	0.9600
CI2A—CI3A	1.3/4 (4)	C29B—H38C	0.9600
CI3A—CI4A	1.364 (5)	C31B—H40	0.9300
CI4A—CI5A	1.368 (5)	C32B—H41	0.9300
C15A—C16A	1.377 (4)	C33B—H42	0.9300
C19A—C20A	1.468 (3)	C34B—H43	0.9300
C20A—C25A	1.389 (3)	C35B—H44	0.9300
C20A—C21A	1.381 (4)	C37B—H46	0.9300
C21A—C22A	1.375 (4)	C38B—H47	0.9300
C22A—C23A	1.377 (4)	C39B—H48	0.9300
C23A—C24A	1.371 (5)	C40B—H49	0.9300
C24A—C25A	1.381 (4)	C41B—H50	0.9300
С4А—Н6С	0.9600	C46B—H60	0.9300
C4A—H6B	0.9600	C47B—H61	0.9300
C4A—H6A	0.9600	C48B—H62	0.9300
С6А—Н8	0.9300	C49B—H63	0.9300
С7А—Н9	0.9300	C50B—H64	0.9300
S1A…O1A	2.704 (2)	C23A…H42 <sup>vii</sup>	3.0000
S1A…N5A	2.557 (2)	C26B···H31 <sup>i</sup>	2.9400
S1A····C34B <sup>i</sup>	3.626 (4)	C27B…H46	3.0000
S2B…O2B <sup>ii</sup>	3.2950 (19)	C28B…H44	2.9800
S2B…N10B	2.555 (2)	C28B····H61 <sup>ii</sup>	3.0400
S2B…O2B	2.7580 (19)	C28B…H53	2.8000
S2B…C13A	3.545 (3)	C29B…H44	2.9100
S1A…H48 <sup>iii</sup>	3.1100	C29B…H53	2.9900
S1A…H32	2.7600	C30B…H38A	2.8300
S2B…H60	2.7000	C31B…H61 <sup>ii</sup>	3.0500
O1A···S1A	2.704 (2)	C31B····H41 <sup>ix</sup>	2.9900
01A…C4A	3.107 (3)	C32B···H40 <sup>ix</sup>	3,1000
02B···S2B	2.7580 (19)	C33B···H30 <sup>vii</sup>	2.9700
02B···S2B <sup>ii</sup>	3 2950 (19)	C35B···H32 <sup>i</sup>	2.8700
02B···C37B	3 184 (3)	C35B…H38C	3 0800
01A…H6B	2.4200	C35B…H38A	3.0000

O1A····H29 <sup>iv</sup>	2.6900	C37B…H16	3.0200
O2B…H46	2.4100	C37B…H17	3.0600
N2A…C29B <sup>iv</sup>	3.450 (3)	C37B····H6A <sup>x</sup>	2.8400
N3…C11A	3.346 (3)	C38B…H16	2.9400
N3…C16A	3.249 (3)	C38B····H6A <sup>x</sup>	2.9800
N3…N9B	2.916 (3)	C40B····H50 <sup>xi</sup>	2.9600
N4A…S1A	2.5522 (19)	C41B····H50 <sup>xi</sup>	2.9800
N4A…N8B	2.902 (3)	C42B…H46	2.8500
N5A…S1A	2.557 (2)	C42B…H38B	2.8500
N5A…C29B	3.443 (3)	C43B…H21	2.9000
N8B…N4A	2.902 (3)	C44B···H12 <sup>v</sup>	2.8700
N8B…C29B	3.304 (4)	C45B…H12 <sup>v</sup>	3.0300
N9B…N3	2.916 (3)	H6A····C38B <sup>vi</sup>	2.9800
N9B…S2B	2.549 (2)	H6A…C5A	2.9800
N9B…C11A	3.373 (3)	H6A····C37B <sup>vi</sup>	2.8400
N10B…S2B	2.555 (2)	H6B…O1A	2.4200
N10B…C12A	3.397 (4)	H6B…C17A	2.7900
N2A…H14	2.6100	H6C…C10A	2.9400
N2A···H8	2.7600	H6C…H12	2.4100
N3…H63 <sup>v</sup>	2.8600	H8…N2A	2.7600
N3…H18	2.8500	H12····C44B <sup>v</sup>	2.8700
N4A…H53	2.0700	H12····C45B <sup>v</sup>	3.0300
N5A…H28	2.6100	H12…H6C	2.4100
N5A···H38C	2.5900	H12···C3A	3.0100
N6B···H61 <sup>ii</sup>	2.8700	H12…C4A	2.9700
N7B···H31 <sup>i</sup>	2.9400	H14…N2A	2.6100
N7B…H40	2.7400	H16C38B	2.9400
N7B…H50	2.6000	H16…C37B	3.0200
N8B···H38B	2.9100	H17···C37B	3.0600
N9B…H21	2.1300	H18…C17A	2.8800
N10B…H64	2.5900	H18N3	2.8500
C4A···C10A	3.282 (4)	H18····C2A	2.9400
C4A···C37B <sup>vi</sup>	3.476 (4)	H21···C1A	2.7800
C4A···O1A	3.107 (3)	H21…C11A	2.8100
C10A···C4A	3.282 (4)	H21N9B	2.1300
C11A···N9B	3.373 (3)	H21···C43B	2.9000
C11AN3	3.346 (3)	H21…C16A	2.8500
C11A····C29B <sup>iv</sup>	3,508 (4)	H28N5A	2.6100
C12AN10B	3.397 (4)	H28…H44	2.5700
C12A…C44B	3.410 (4)	H29····O1A <sup>viii</sup>	2.6900
C13A···S2B	3.545 (3)	H30····C33B <sup>vii</sup>	2.9700
C14A…C37B	3.571 (5)	H30…H42 <sup>vii</sup>	2.5700
C15A···C37B	3,592 (4)	$H31\cdots N7B^{i}$	2.9400
C16A…C17A	3.419 (4)	H31C26B <sup>i</sup>	2.9400
C16AN3	3.249 (3)	H32…H44 <sup>i</sup>	2.5600
C17A…C16A	3 419 (4)	H32····S1A	2.5000
$C17A \cdots C49B^{v}$	3.590 (4)	H32C35Bi	2.8700
C18A····C24A <sup>i</sup>	3.548 (3)	H38A····C11A <sup>viii</sup>	2.7600

	/->		
C19A····C24A <sup>1</sup>	3.592 (3)	H38A···C12 $A$ <sup>viii</sup>	3.0000
C19A···C25A <sup>i</sup>	.358 (3) H38A…C16A <sup>viii</sup>		2.9600
C23A····C33B <sup>vii</sup>	3.599 (6)	H38A…C30B	2.8300
C24A····C18A <sup>i</sup>	3.548 (3)	H38A…C35B	3.0000
C24A····C19A <sup>i</sup>	3.592 (3)	H38B…N8B	2.9100
C25A····C19A <sup>i</sup>	3.358 (3)	H38B…C42B	2.8500
C29B…C35B	3.239 (4)	H38C…N5A	2.5900
C29B…N2A <sup>viii</sup>	3.450 (3)	H38C…C35B	3.0800
C29B…N5A	3.443 (3)	H38C…H44	2.5000
C29B····C11A <sup>viii</sup>	3.508 (4)	H40…N7B	2.7400
C29B…N8B	3.304 (4)	H40····C32B <sup>ix</sup>	3.1000
C31B····C32B <sup>ix</sup>	3.441 (5)	H41····C31B <sup>ix</sup>	2.9900
C32B····C31B <sup>ix</sup>	3.441 (5)	H42…C22A <sup>vii</sup>	3.0200
C32B····C32B <sup>ix</sup>	3.577 (5)	H42····C23A <sup>vii</sup>	3.0000
C33B····C23A <sup>vii</sup>	3.599 (6)	H42…H30 <sup>vii</sup>	2.5700
C34B···S1A <sup>i</sup>	3.626 (4)	H44…C21A	3.0100
C35B···C29B	3.239 (4)	H44…C28B	2.9800
C37B…C15A	3 592 (4)	H44C29B	2.9100
C37B···C14A	3 571 (5)	H44···H28	2 5700
C37B···C4A <sup>x</sup>	3,476(4)	H44H38C	2.5700
C37B…O2B	3 184 (3)	H44H32i	2.5600
C37B…C42B	3 366 (4)	H4602B	2.3000
C42BC37B	3 366 (4)	H46C27B	3 0000
C44BC12A	3.300(4)	H46C42B	2 8500
$C_{44}D^{-}C_{12}A^{-}$	3,500 (4)	$H_{48}$ S1 $A^{xii}$	2.8500
$C149B^{-1}C1/A$	2 7800	H40H50xi	2 3600
	2.7800	H49N7D	2.5000
C2A112	2.9400		2.0000
C4A 1112	2.0700	H50 C41Dxi	2.9000
C4A···H12	2.9700	H50-1140xi	2.9800
СЗАНбА	2.9800	H50····H49 <sup>xi</sup>	2.3600
CIUA···H6C	2.9400	H50····H50**	2.4000
CIIA···H2I	2.8100	H53…N4A	2.0700
	2.7600	H53····C18A	2.9900
С12А…Н38А <sup>т</sup>	3.0000	H53C28B	2.8000
C16A····H38A <sup>IV</sup>	2.9600	Н53…С29В	2.9900
С16А…Н21	2.8500	H60····S2B	2.7000
С17А…Н6В	2.7900	H61···N6B <sup>ii</sup>	2.8700
C17A…H18	2.8800	H61···C28B <sup>ii</sup>	3.0400
C18A…H53	2.9900	H61···C31B <sup>ii</sup>	3.0500
C21A…H44	3.0100	H63…N3 <sup>v</sup>	2.8600
C22A····H42 <sup>vii</sup>	3.0200	H64…N10B	2.5900
C18A S1A C10A	86 67 (11)	С20А С21А Ц29	120.00
$C_{10A} = S_{1A} = C_{19A}$	00.07(11)	$C_{20A} = C_{21A} = \Pi_{20}$	120.00
$ \begin{array}{c} \mathbf{U}_{43}\mathbf{D}_{}\mathbf{S}_{2}\mathbf{D}_{}\mathbf{U}_{44}\mathbf{B} \\ \mathbf{W}_{24}  \mathbf{W}_{14}  \mathbf{C}_{24} \\ \end{array} $	00.22(11)	$C_{22}A \rightarrow C_{21}A \rightarrow H_{20}$	120.00
$N2A \rightarrow N1A \rightarrow C5A$	112.4 (2)	$C_{21A} = C_{22A} = H_{29}$	120.00
NZA-NIA-CSA	11/.//(19)	$C_{23}A - C_{22}A - H_{29}$	120.00
USA-NIA-USA	129.9 (2)	$C_{22}A - C_{23}A - H_{30}$	120.00
NIA—N2A—CIA	105.28 (19)	C24A—C23A—H30	120.00

C17A—N3—C18A	123.55 (19)	C23A—C24A—H31	120.00
N5A—N4A—C18A	112.18 (18)	C25A—C24A—H31	120.00
N4A—N5A—C19A	112.3 (2)	С20А—С25А—Н32	120.00
C17A—N3—H21	118.00	С24А—С25А—Н32	120.00
C18A—N3—H21	118.00	N7B—C26B—C27B	110.2 (2)
N7B—N6B—C28B	112.5 (2)	N7B—C26B—C36B	118.8 (2)
C28B—N6B—C30B	128.8 (2)	C27B—C26B—C36B	130.9 (2)
N7B—N6B—C30B	118.65 (19)	C26B—C27B—C28B	106.27 (19)
N6B—N7B—C26B	105.50 (18)	C28B—C27B—C42B	124.3 (2)
C42B—N8B—C43B	124.31 (19)	C26B—C27B—C42B	129.5 (2)
N10B—N9B—C43B	111.92 (18)	N6B-C28B-C29B	123.4 (2)
N9B—N10B—C44B	112.3 (2)	N6B-C28B-C27B	105.5 (2)
C43B—N8B—H53	118.00	C27B—C28B—C29B	130.9 (2)
C42B—N8B—H53	118.00	N6B-C30B-C35B	120.0 (2)
N2A—C1A—C2A	110.8 (2)	N6B-C30B-C31B	119.2 (2)
N2A—C1A—C11A	117.8 (2)	C31B—C30B—C35B	120.8 (3)
C2A—C1A—C11A	131.2 (2)	C30B—C31B—C32B	119.0 (3)
C1A—C2A—C17A	131.4 (2)	C31B—C32B—C33B	120.5 (4)
C3A—C2A—C17A	123.1 (2)	C32B—C33B—C34B	120.2 (4)
C1A—C2A—C3A	105.3 (2)	C33B—C34B—C35B	120.6 (3)
N1A—C3A—C2A	106.2 (2)	C30B—C35B—C34B	119.0 (3)
C2A—C3A—C4A	130.6 (2)	C37B—C36B—C41B	118.0 (2)
N1A—C3A—C4A	123.2 (2)	C26B—C36B—C37B	122.6 (2)
N1A—C5A—C10A	120.7 (2)	C26B—C36B—C41B	119.4 (2)
N1A—C5A—C6A	118.7 (2)	C36B—C37B—C38B	120.3 (2)
C6A—C5A—C10A	120.5 (2)	C37B—C38B—C39B	121.0 (3)
C5A—C6A—C7A	119.2 (3)	C38B—C39B—C40B	119.1 (3)
C6A—C7A—C8A	120.1 (3)	C39B—C40B—C41B	120.6 (3)
C7A—C8A—C9A	120.3 (3)	C36B—C41B—C40B	121.0 (3)
C8A—C9A—C10A	120.4 (3)	O2B—C42B—C27B	124.8 (2)
C5A—C10A—C9A	119.4 (3)	O2B—C42B—N8B	120.8 (2)
C1A—C11A—C12A	119.9 (2)	N8B—C42B—C27B	114.41 (19)
C1A—C11A—C16A	122.1 (2)	N8B—C43B—N9B	120.20 (19)
C12A—C11A—C16A	117.8 (2)	S2B—C43B—N9B	115.12 (16)
C11A—C12A—C13A	120.7 (2)	S2B—C43B—N8B	124.67 (17)
C12A—C13A—C14A	120.5 (3)	S2B-C44B-N10B	114.43 (17)
C13A—C14A—C15A	120.1 (3)	S2B—C44B—C45B	122.50 (18)
C14A—C15A—C16A	119.9 (3)	N10B—C44B—C45B	123.0 (2)
C11A—C16A—C15A	121.1 (2)	C44B—C45B—C46B	120.8 (2)
O1A—C17A—C2A	123.8 (2)	C46B—C45B—C50B	118.7 (2)
N3—C17A—C2A	116.2 (2)	C44B—C45B—C50B	120.5 (2)
O1A—C17A—N3	119.9 (2)	C45B—C46B—C47B	120.9 (3)
S1A—C18A—N4A	114.62 (17)	C46B—C47B—C48B	119.9 (3)
S1A-C18A-N3	124.69 (17)	C47B—C48B—C49B	119.9 (3)
N3—C18A—N4A	120.63 (19)	C48B—C49B—C50B	121.2 (3)
S1A—C19A—C20A	123.10 (17)	C45B—C50B—C49B	119.4 (3)
N5A-C19A-C20A	122.7 (2)	C28B—C29B—H38A	109.00
S1A—C19A—N5A	114.24 (18)	C28B—C29B—H38B	109.00

C21A—C20A—C25A	118.5 (2)	C28B—C29B—H38C	109.00
C19A—C20A—C25A	120.8 (2)	H38A—C29B—H38B	110.00
C19A—C20A—C21A	120.7 (2)	H38A—C29B—H38C	109.00
C20A—C21A—C22A	120.7 (2)	H38B—C29B—H38C	109.00
C21A—C22A—C23A	120.3 (3)	C30B—C31B—H40	120.00
C22A—C23A—C24A	119.9 (3)	C32B—C31B—H40	121.00
C23A—C24A—C25A	119.9 (2)	C31B—C32B—H41	120.00
C20A—C25A—C24A	120.7 (3)	C33B—C32B—H41	120.00
СЗА—С4А—Н6В	110.00	C32B—C33B—H42	120.00
СЗА—С4А—Н6А	110.00	C34B—C33B—H42	120.00
H6A—C4A—H6C	109.00	C33B—C34B—H43	120.00
C3A - C4A - H6C	110.00	C35B-C34B-H43	120.00
H6B-C4A-H6C	109.00	C30B $C35B$ $H44$	120.00
H6A - C4A - H6B	109.00	C34B— $C35B$ — $H44$	121.00
$C_{5A}$ $C_{6A}$ $H_8$	120.00	$C_{36B}$ $C_{37B}$ $H_{46}$	121.00
C7A - C6A - H8	120.00	$C_{38B}$ $C_{37B}$ $H_{46}$	120.00
C6A C7A H9	120.00	$\begin{array}{c} C_{37B} \\ C_{37B} \\ C_{38B} \\ H_{47} \\ H_$	110.00
C8A C7A H9	120.00	$C_{30B} = C_{38B} = H47$	120.00
$C_{0A} = C_{A} = H_{10}$	120.00	$C_{39D} = C_{30D} = H_{47}$	120.00
C7A C8A H10	120.00	$C_{30} = C_{30} = C$	120.00
$C_{A} = C_{A} = H_{10}$	120.00	C40D - C39D - H40	121.00
$C_{10A} - C_{9A} - H_{11}$	120.00	$C_{39}B - C_{40}B - H_{49}$	120.00
	120.00	C41B - C40B - H49 $C26B - C41B - H50$	120.00
$C_{\text{SA}} = C_{10A} = H_{12}$	120.00	C30B - C41B - H50	120.00
$C_{11A} = C_{12A} = H_{12}$	120.00	C40B - C41B - H50	119.00
C12A = C12A = H14	120.00	C45B - C46B - H60	120.00
C13A - C12A - H14	120.00	C4/B - C40B - H00	120.00
C12A = C12A = H15	120.00	C40B - C47B - H61	120.00
C12A - C13A - H15	120.00	C48B - C4/B - H61	120.00
C13A - C14A - H16	120.00	C4/B - C48B - H62	120.00
CI5A—CI4A—HI6	120.00	C49B—C48B—H62	120.00
C14A—C15A—H17	120.00	C48B—C49B—H63	119.00
C16A—C15A—H17	120.00	C50B—C49B—H63	119.00
C11A—C16A—H18	119.00	C45B—C50B—H64	120.00
C15A—C16A—H18	120.00	C49B—C50B—H64	120.00
C10A S1A C18A N2	176 2 (2)		-0.5 (4)
C10A = S1A = C18A = N4A	1/0.2(2) -0.07(18)	$C_{10A} = C_{3A} = C_{0A} = C_{7A}$	0.3(4)
C19A = S1A = C10A = N4A	-0.97(18)	$C_{A} = C_{A} = C_{A} = C_{A}$	1.3(4)
C18A = S1A = C19A = N3A	0.81(18)	COA - C/A - COA - CIA	-0.3(3)
$C_{10}A = S_{10}A = C_{10}A = C_{20}A$	1/9.8(2)	$C^{A}$ $C^{A$	-1.2(3)
C44B = S2B = C44B = N10B	0.40(19)	$C_{0}A = C_{0}A = C_{0}A = C_{0}A$	1.9(4)
C43B = S2B = C44B = N10B	-0.4(2)	CIA - CIIA - CI2A - CI3A	1/5.2 (3)
C44B = S2B = C43B = N8B	1/9.6 (2)	C12A— $C11A$ — $C16A$ — $C13A$	0.0(4)
$C_{43}B = S_{2}B = C_{44}B = C_{45}B$	1/0.8 (2)	CIDA - CIIA - CIZA - CIZA	0.2 (4)
C5A NIA N2A CIA	1.9 (3)	CIA - CIA - CI6A - CI5A	-1/4.9(2)
USA-NIA-NZA-UIA	-1/8.3(2)	C11A - C12A - C13A - C14A	-0.2(5)
$N_{2}A - N_{1}A - C_{2}A - C_{6}A$	-50.4(3)	C12A - C13A - C14A - C15A	0.0(5)
NZA—NIA—C5A—C10A	125.7 (2)	U13A—U14A—U15A—U16A	0.2 (5)
C3A—NIA—C5A—C6A	129.4 (3)	CI4A—CI5A—CI6A—CI1A	-0.2 (4)

C3A—N1A—C5A—C10A	-54.5 (3)	S1A—C19A—C20A—C25A	-14.8 (3)
N2A—N1A—C3A—C4A	177.5 (2)	N5A-C19A-C20A-C21A	-15.3 (3)
C5A—N1A—C3A—C2A	178.2 (2)	S1A-C19A-C20A-C21A	165.70 (19)
N2A—N1A—C3A—C2A	-2.1 (3)	N5A—C19A—C20A—C25A	164.1 (2)
C5A—N1A—C3A—C4A	-2.3 (4)	C21A—C20A—C25A—C24A	0.0 (3)
N1A—N2A—C1A—C2A	-1.0(3)	C25A—C20A—C21A—C22A	-0.7 (4)
N1A—N2A—C1A—C11A	-176.1 (2)	C19A—C20A—C25A—C24A	-179.5 (2)
C18A—N3—C17A—O1A	4.2 (4)	C19A—C20A—C21A—C22A	178.8 (2)
C18A—N3—C17A—C2A	-172.8 (2)	C20A—C21A—C22A—C23A	1.0 (4)
C17A—N3—C18A—S1A	6.7 (3)	C21A—C22A—C23A—C24A	-0.5(4)
C17A—N3—C18A—N4A	-176.3 (2)	C22A—C23A—C24A—C25A	-0.1 (4)
N5A—N4A—C18A—S1A	0.9 (2)	C23A—C24A—C25A—C20A	0.4 (4)
N5A—N4A—C18A—N3	-176.42(19)	N7B—C26B—C27B—C28B	0.0 (3)
C18A—N4A—N5A—C19A	-0.3(3)	N7B—C26B—C27B—C42B	179.6 (2)
N4A—N5A—C19A—S1A	-0.5(2)	C36B—C26B—C27B—C28B	-176.1(2)
N4A - N5A - C19A - C20A	-17952(19)	$C_{36B} - C_{26B} - C_{27B} - C_{42B}$	3 5 (4)
$C_{28B}$ N6B N7B $C_{26B}$	01(3)	N7B-C26B-C36B-C37B	1481(2)
N7B—N6B—C28B—C29B	1751(2)	N7B - C26B - C36B - C41B	-315(3)
C30B - N6B - N7B - C26B	173.1(2) 177.6(2)	$C_{27B} - C_{26B} - C_{36B} - C_{37B}$	-36.2(4)
N7B_N6B_C28B_C27B	-0.1(3)	$C_{27B} = C_{26B} = C_{36B} = C_{41B}$	144.3(3)
N7B-N6B-C30B-C31B	-480(3)	$C_{26B} = C_{20B} = C_{30B} = C_{41B}$	0.1(3)
N7B N6B C30B C35B	1200(3)	$C_{20} = C_{27} = C_{20} = C_{20} = C_{20}$	-174.7(2)
$\begin{array}{c} 1170 \\ 1100 \\ 11$	129.0(3) 1201(3)	$C_{20}D - C_{27}D - C_{28}D - C_{29}D$	-179.6(2)
$C_{28} = N6 = C_{20} = C_{25} = C_{25}$	-54.0(4)	C42D - C27D - C28D - N0D	1/9.0(2)
$C_{20}$ NGP $C_{20}$ C27P	-34.0(4)	$C_{42B} - C_{27B} - C_{28B} - C_{29B}$	5.7(4)
$C_{30B} = NOB = C_{20B} = C_{20B}$	-1/7.3(2)	$C_{20}B - C_{27}B - C_{42}B - O_{28}B$	39.4 (4)
$C_{30B}$ NOB $C_{28B}$ $C_{29B}$	-2.1(4)	$C_{20B} = C_{27B} = C_{42B} = N_{8B}$	-122.2(3)
NOB - N/B - C2OB - C2/B	0.0(3)	$C_{28B} = C_{27B} = C_{42B} = O_{2B}$	-121.1(3)
N0B - N/B - C20B - C30B	1/6.5(2)	$C_{28B} - C_{27B} - C_{42B} - N_{8B}$	57.4 (3)
C42B—N8B—C43B—S2B	14.2 (3)	N6B-C30B-C31B-C32B	1/6.1 (3)
C43B— $N8B$ — $C42B$ — $C27B$	1/8.2 (2)	C35B—C30B—C31B—C32B	-0.8 (4)
C42B—N8B—C43B—N9B	-166.7 (2)	N6B—C30B—C35B—C34B	-175.8 (3)
C43B—N8B—C42B—O2B	-3.3 (4)	C31B—C30B—C35B—C34B	1.1 (4)
N10B—N9B—C43B—S2B	-0.5 (3)	C30B—C31B—C32B—C33B	-0.6 (5)
N10B—N9B—C43B—N8B	-179.7 (2)	C31B—C32B—C33B—C34B	1.7 (5)
C43B—N9B—N10B—C44B	0.2 (3)	C32B—C33B—C34B—C35B	-1.4 (6)
N9B—N10B—C44B—S2B	0.2 (3)	C33B—C34B—C35B—C30B	0.1 (5)
N9B—N10B—C44B—C45B	-176.9 (2)	C26B—C36B—C37B—C38B	-178.2 (2)
N2A—C1A—C2A—C3A	-0.2 (3)	C41B—C36B—C37B—C38B	1.3 (4)
N2A—C1A—C2A—C17A	174.5 (2)	C26B—C36B—C41B—C40B	178.3 (3)
C11A—C1A—C2A—C3A	174.1 (2)	C37B—C36B—C41B—C40B	-1.3 (5)
C2A—C1A—C11A—C12A	154.8 (3)	C36B—C37B—C38B—C39B	-0.8 (4)
C2A—C1A—C11A—C16A	-30.5 (4)	C37B—C38B—C39B—C40B	0.1 (5)
N2A—C1A—C11A—C16A	143.4 (2)	C38B—C39B—C40B—C41B	0.0 (5)
C11A—C1A—C2A—C17A	-11.2 (4)	C39B—C40B—C41B—C36B	0.6 (6)
N2A—C1A—C11A—C12A	-31.3 (3)	S2B-C44B-C45B-C46B	-2.4 (4)
C1A—C2A—C3A—C4A	-178.2 (2)	S2B-C44B-C45B-C50B	178.7 (2)
C1A—C2A—C17A—O1A	147.2 (3)	N10B—C44B—C45B—C46B	174.4 (3)
C17A—C2A—C3A—N1A	-174.0 (2)	N10B—C44B—C45B—C50B	-4.5 (4)

Symmetry codes: (i) -*x*+2, -*y*+1, -*z*; (ii) -*x*+2, -*y*, -*z*+1; (iii) *x*, *y*+1, *z*; (iv) *x*-1, *y*, *z*; (v) -*x*+1, -*y*+1, -*z*+1; (vi) *x*-1, *y*+1, *z*; (vii) -*x*+3, -*y*+1, -*z*; (viii) *x*+1, *y*, *z*; (ix) -*x*+3, -*y*, -*z*; (x) *x*+1, *y*-1, *z*; (xii) -*x*+2, -*y*, -*z*; (xii) *x*, *y*-1, *z*.

*Hydrogen-bond geometry (Å, °)* 

D—H···A	D—H	Н…А	D····A	D—H···A
N3—H21…N9B	0.86	2.13	2.916 (3)	151
N8 <i>B</i> —H53…N4 <i>A</i>	0.86	2.07	2.902 (3)	163
C4 <i>A</i> —H6 <i>B</i> ····O1 <i>A</i>	0.96	2.42	3.107 (3)	128
C29 <i>B</i> —H38 <i>C</i> ···N5 <i>A</i>	0.96	2.59	3.443 (3)	148
C37 <i>B</i> —H46····O2 <i>B</i>	0.93	2.41	3.184 (3)	141