# organic compounds

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# {2-[(4-Nitrobenzylidene)amino]-4,5,6,7tetrahydro-1-benzothiophen-3-yl}-(phenyl)methanone

### Manpreet Kaur,<sup>a</sup> Jerry P. Jasinski,<sup>b</sup>\* Channappa N. Kavitha,<sup>a</sup> H. S. Yathirajan<sup>a</sup> and K. Byrappa<sup>c</sup>

<sup>a</sup>Department of Studies in Chemistry, University of Mysore, Manasagangotri, Mysore 570 006, India, <sup>b</sup>Department of Chemistry, Keene State College, 229 Main Street, Keene, NH 03435-2001, USA, and <sup>c</sup>Materials Science Center, University of Mysore, Vijyana Bhavan Building, Manasagangothri, Mysore 570 006, India Correspondence e-mail: jjasinski@keene.edu

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Key indicators: single-crystal X-ray study; T = 173 K; mean  $\sigma$ (C–C) = 0.004 Å; disorder in main residue; R factor = 0.035; wR factor = 0.090; data-to-parameter ratio = 10.6

In the title compound,  $C_{22}H_{18}N_2O_3S$ , disorder is found in the benzovl group (A and B), as well as for four C atoms of the cyclohexene ring. Two orientations were modeled in a 0.583 (5):0.417 (5) ratio. The cyclohexene ring is in a distorted chair conformation. The dihedral angles between the mean plane of the thiophene ring and the 4-nitrobenzene and phenyl rings are 30.9 (8) and 64.8 (3) (A) and 62.4 (7) $^{\circ}$  (B). The mean planes of the 4-nitrobenzene and the phenyl rings are almost perpendicular to each other, with dihedral angles of 85.4 (1) (A) and 83.9 (8)° (B). An extensive array of weak C-H···O interactions consolidate molecules into a three-dimensional architecture, forming chains along [001] and [010] and layers parallel to (011).

### **Related literature**

For applications of 2-aminothiophene derivatives in pesticides, dyes and pharmaceuticals, see: Puterová et al. (2010). For the biological and industrial importance of Schiff bases, see: Desai et al. (2001); Karia & Parsania (1999); Samadhiya & Halve (2001); Singh & Dash (1988). For Schiff bases utilized as starting materials in the synthesis of compounds of industrial and biological interest, see: Aydogan et al. (2001); Taggi et al. (2002). For related structures, see: Kaur *et al.* (2014a,b); Kubicki et al. (2012). For puckering parameters, see: Cremer & Pople (1975).



V = 955.39 (4) Å<sup>3</sup>

Cu  $K\alpha$  radiation

 $0.24 \times 0.18 \times 0.06 \text{ mm}$ 

6206 measured reflections

2781 independent reflections 2610 reflections with  $I > 2\sigma(I)$ 

 $\mu = 1.72 \text{ mm}^{-1}$ 

T = 173 K

 $R_{\rm int} = 0.027$ 

Z = 2

### **Experimental**

### Crystal data

C22H18N2O3S  $M_r = 390.44$ Monoclinic, P21 a = 4.61595 (13) Å b = 17.6844 (4) Å c = 11.7068 (3) Å  $\beta = 91.285 (3)^{\circ}$ 

### Data collection

Agilent Eos Gemini diffractometer Absorption correction: multi-scan (CrysAlis PRO and CrysAlis RED; Agilent, 2012)  $T_{\min} = 0.634, T_{\max} = 1.000$ 

### Refinement

$R[F^2 > 2\sigma(F^2)] = 0.035$	$\Delta \rho_{\rm min} = -0.19 \ {\rm e} \ {\rm \AA}^{-3}$
$wR(F^2) = 0.090$	Absolute structure: Flack x
S = 1.02	determined using 764 quotients
2781 reflections	$[(I^+)-(I^-)]/[(I^+)+(I^-)]$
263 parameters	(Parsons & Flack, 2004)
138 restraints	Absolute structure parameter:
H-atom parameters constrained	0.028 (16)
$\Delta \rho_{\rm max} = 0.21 \ {\rm e} \ {\rm \AA}^{-3}$	

# Table 1

H	yd	lrogen-	bond	geometr	у (	(Α,	0)	).
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$D - H \cdots A$	D-H	$H \cdots A$	$D \cdots A$	$D - \mathbf{H} \cdot \cdot \cdot A$
$C4A - H4AA \cdots O1B^{i}$	0.99	2.38	3.15 (4)	135
$C4B - H4BA \cdots O1A^{i}$	0.99	2.50	3.45 (4)	162
$C4B - H4BA \cdots O1B^{i}$	0.99	2.26	3.18 (4)	154
$C7B - H7BB \cdots O2^{ii}$	0.99	2.46	3.44 (3)	169
$C13B - H13B \cdot \cdot \cdot O3^{iii}$	0.95	2.55	3.371 (13)	145
$C21 - H21 \cdots O1A^{iv}$	0.95	2.40	3.127 (18)	133
$C21 - H21 \cdots O1B^{iv}$	0.95	2.44	3.13 (3)	129
				1 (1)

Symmetry codes: (i) x + 1, y, z; (ii) x + 1, y, z + 1; (iii)  $-x - 1, y - \frac{1}{2}, -z$ ; (iv)  $-x - 1, y + \frac{1}{2}, -z + 1.$ 

Data collection: CrysAlis PRO (Agilent, 2012); cell refinement: CrysAlis PRO; data reduction: CrysAlis RED (Agilent, 2012); program(s) used to solve structure: SUPERFLIP (Palatinus & Chapuis, 2007); program(s) used to refine structure: SHELXL2012 (Sheldrick, 2008); molecular graphics: OLEX2 (Dolomanov et al., 2009); software used to prepare material for publication: OLEX2.

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Supporting information for this paper is available from the IUCr electronic archives (Reference: TK5318).

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# supporting information

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# {2-[(4-Nitrobenzylidene)amino]-4,5,6,7-tetrahydro-1-benzothiophen-3-yl} (phenyl)methanone

# Manpreet Kaur, Jerry P. Jasinski, Channappa N. Kavitha, H. S. Yathirajan and K. Byrappa

### S1. Structural commentary

2-Aminothiophene derivatives have been used in a number of applications, such as in pesticides, dyes and pharmaceuticals. A review on the synthesis and properties of these compounds has been reported (Puterová *et al.*, 2010). Schiff base compounds are an important class of compounds, both synthetically and biologically. These compounds show biological activities including anti-bacterial, anti-fungal, anti-cancer and herbicidal (Desai *et al.*, 2001; Karia & Parsania, 1999; Samadhiya & Halve, 2001; Singh & Dash, 1988). Furthermore, Schiff bases are utilized as starting materials in the synthesis of compounds of industrial (Aydogan *et al.*, 2001) and biological interest such as  $\beta$ -lactams (Taggi *et al.*, 2002). Some of the recently reported Schiff base structures of 2-aminothiophenes by our group include {2-[(2-hydroxybenzylidene)amino]-4,5,6,7-tetrahydro-1-benzothiophene-3-yl} (phenyl)methanone (Kaur *et al.*, 2014*a*) and [2-benzylideneamino)-4,5,6,7-tetrahydro benzo[b]thiophene-3-yl](phenyl) methanone (Kaur *et al.*, 2014*b*). Also, the crystal and molecular structures of two 2-aminothiophenes have been previously reported by our group (Kubicki *et al.*, 2012). In continuation of our work on 2-aminothiophenes and Schiff bases, we report here the crystal structure of the title compound, (I).

In (I), the cyclohexene ring is in a distorted chair conformation with four carbon atoms disordered over two sets of sites with an occupancy ratio of 0.583 (5): 0.417 (5) (Fig. 1). Puckering parameters C3/C4A—C7A/C8: Q and  $\varphi = 0.511$  (4) Å and 157.387 (6)°, and C3/C4B—C7B/C8: Q and  $\varphi = 0.483$  (8) Å and 212.306 (8)° (Cremer & Pople, 1975). The disorder extends to the benzoyl residue (A & B). The dihedral angles between the mean plane of the thiophene ring and the 4-nitrophenyl and the phenyl rings is 30.9 (8) and 64.8 (3) (A) and 62.4 (7)° (B), respectively. The mean planes of 4-nitrophenyl and the phenyl rings are almost perpendicular to each other with a dihedral angle of 85.4 (1) (A) and 83.9 (8)° (B). An extensive array of weak C—H…O intermolecular interactions leads to a 3-D architecure, forming chains along [001] and [010] and layers parallel to (011) (Fig. 2).

### S2. Synthesis and crystallization

To a solution of (2-amino-4,5,6,7-tetrahydro-benzo[b]thiophen-3-yl)- phenyl-methanone (200 mg, 0.79 mmol) in 10 ml of methanol an equimolar amount of 4-nitrobenzaldehyde (120 mg, 0.79 mmol) was added with constant stirring. The mixture was refluxed for 3 h. A yellow precipitate was obtained. Completion of the reaction was confirmed by TLC. The precipitate was filtered and dried at room temperature overnight. The solid was recrystallized using ethylacetate and the crystals were used as such for x-ray diffraction studies.

### S3. Refinement

The H atoms were placed in their calculated positions and then refined using the riding model with Atom—H lengths of 0.93 Å (CH) or 0.97 Å (CH<sub>2</sub>), and with U<sub>iso</sub> set to  $1.2U_{eq}$  of the parent atom. Disorder was modeled for C4A—C7A and

C4B—C7B of the cyclohexane ring, C10A—C15A/O1A and C10B—C15B/O1B of the benzoyl group over two positions with an occupancy ratio of 0.583 (5):0.417 (5).



## Figure 1

ORTEP drawing of (I) showing the labeling scheme and 30% probability displacement ellipsoids (major and minor components of the disordered atoms in the cyclohexane, benzoyl groups are displayed with dashed lines).



## Figure 2

Molecular packing for (I) viewed along the b axis. Dashed lines indicate weak C—H…O intermolecular interactions. H atoms not involved in the weak intermolecular interactions have been removed for clarity.

## {2-[(4-Nitrobenzylidene)amino]-4,5,6,7-tetrahydro-1-benzothiophen-3-yl}(phenyl)methanone

F(000) = 408
$D_{\rm x} = 1.357 {\rm ~Mg} {\rm ~m}^{-3}$
Cu <i>K</i> $\alpha$ radiation, $\lambda = 1.54184$ Å
Cell parameters from 3146 reflections
$\theta = 4.5 - 71.4^{\circ}$
$\mu = 1.72 \text{ mm}^{-1}$
T = 173  K
Irregular, yellow
$0.24 \times 0.18 \times 0.06 \text{ mm}$
6206 measured reflections
2781 independent reflections
2610 reflections with $I > 2\sigma(I)$
$R_{\rm int} = 0.027$
$\theta_{\text{max}} = 71.1^{\circ},  \theta_{\text{min}} = 3.8^{\circ}$
$h = -5 \rightarrow 5$
$k = -18 \rightarrow 21$
$l = -11 \rightarrow 14$

Refinement

Refinement on $F^2$	H-atom parameters constrained
Least-squares matrix: full	$w = 1/[\sigma^2(F_o^2) + (0.0608P)^2]$
$R[F^2 > 2\sigma(F^2)] = 0.035$	where $P = (F_o^2 + 2F_c^2)/3$
$wR(F^2) = 0.090$	$(\Delta/\sigma)_{\rm max} < 0.001$
S = 1.02	$\Delta \rho_{\rm max} = 0.21 \text{ e} \text{ Å}^{-3}$
2781 reflections	$\Delta \rho_{\min} = -0.19 \text{ e} \text{ Å}^{-3}$
263 parameters	Absolute structure: Flack x determined using
138 restraints	764 quotients $[(I^+)-(I^-)]/[(I^+)+(I^-)]$ (Parsons &
Primary atom site location: structure-invariant	Flack, 2004)
direct methods	Absolute structure parameter: 0.028 (16)
Hydrogen site location: mixed	

### Special details

**Geometry**. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(\mathring{A}^2)$ 

	x	у	Z	$U_{ m iso}$ */ $U_{ m eq}$	Occ. (<1)
S1	0.24441 (14)	0.70387 (3)	0.62913 (5)	0.03214 (17)	
01A	0.009 (2)	0.4397 (10)	0.5799 (16)	0.041 (2)	0.583 (5)
O1B	-0.071 (4)	0.4474 (15)	0.576 (2)	0.041 (2)	0.417 (5)
02	-0.9787 (6)	0.75162 (18)	-0.0143 (2)	0.0605 (7)	
03	-1.1148 (6)	0.84877 (16)	0.0802 (2)	0.0551 (7)	
N1	-0.0687 (5)	0.64901 (14)	0.44225 (18)	0.0293 (5)	
N2	-0.9655 (6)	0.79235 (16)	0.0691 (2)	0.0385 (6)	
C1	0.0964 (6)	0.49027 (16)	0.5199 (2)	0.0338 (6)	
C2	0.1876 (6)	0.56264 (16)	0.5745 (2)	0.0280 (5)	
C3	0.3469 (6)	0.56491 (16)	0.6813 (2)	0.0303 (6)	
C4A	0.439 (6)	0.4943 (15)	0.7449 (16)	0.0392 (15)	0.583 (5)
H4AA	0.5141	0.4559	0.6915	0.047*	0.583 (5)
H4AB	0.2683	0.4731	0.7832	0.047*	0.583 (5)
C5A	0.6700 (13)	0.5148 (4)	0.8363 (5)	0.0438 (11)	0.583 (5)
H5AA	0.7031	0.4720	0.8895	0.053*	0.583 (5)
H5AB	0.8537	0.5248	0.7969	0.053*	0.583 (5)
C6A	0.5854 (15)	0.5850 (4)	0.9033 (5)	0.0428 (12)	0.583 (5)
H6AA	0.3961	0.5767	0.9394	0.051*	0.583 (5)
H6AB	0.7322	0.5949	0.9644	0.051*	0.583 (5)
C7A	0.578 (5)	0.6541 (8)	0.8218 (18)	0.035 (2)	0.583 (5)
H7AA	0.4883	0.6968	0.8628	0.042*	0.583 (5)
H7AB	0.7767	0.6695	0.8023	0.042*	0.583 (5)
C4B	0.464 (8)	0.502 (2)	0.754 (2)	0.0392 (15)	0.417 (5)
H4BA	0.6486	0.4861	0.7197	0.047*	0.417 (5)
H4BB	0.3324	0.4574	0.7522	0.047*	0.417 (5)
C5B	0.5365 (19)	0.5254 (5)	0.8763 (7)	0.0438 (11)	0.417 (5)
H5BA	0.3503	0.5333	0.9149	0.053*	0.417 (5)
H5BB	0.6429	0.4844	0.9169	0.053*	0.417 (5)

C6B	0.717 (2)	0.5966 (5)	0.8813 (8)	0.0428 (12)	0.417 (5)
H6BA	0.7592	0.6094	0.9623	0.051*	0.417 (5)
H6BB	0.9050	0.5874	0.8443	0.051*	0.417 (5)
C7B	0.551 (7)	0.6653 (12)	0.830 (3)	0.035 (2)	0.417 (5)
H7BA	0.6977	0.7031	0.8078	0.042*	0.417 (5)
H7BB	0.4169	0.6895	0.8834	0.042*	0.417 (5)
C8	0.3991 (6)	0.63650(17)	0.7187 (2)	0.0310(6)	~ /
С9	0.1092 (6)	0.63358 (15)	0.5361 (2)	0.0276 (6)	
C10A	0.1914 (17)	0.4696 (6)	0.4023 (7)	0.0261 (15)	0.583 (5)
C11A	0.0684 (16)	0.4049 (6)	0.3543 (9)	0.0430 (17)	0.583 (5)
H11A	-0.0653	0.3758	0.3964	0.052*	0.583 (5)
C12A	0.1411 (17)	0.3828 (5)	0.2446 (9)	0.049 (2)	0.583 (5)
H12A	0.0571	0.3386	0.2118	0.059*	0.583 (5)
C13A	0.3367 (16)	0.4254 (6)	0.1830(7)	0.050(2)	0.583 (5)
H13A	0.3864	0.4103	0.1081	0.060*	0.583 (5)
C14A	0.4597 (16)	0.4901 (5)	0.2311 (9)	0.051 (2)	0.583 (5)
H14A	0.5934	0.5192	0.1889	0.061*	0.583 (5)
C15A	0.3870 (18)	0.5122 (5)	0.3407 (9)	0.0347 (17)	0.583 (5)
H15A	0.4711	0.5564	0.3735	0.042*	0.583 (5)
C10B	0.127 (3)	0.4756 (10)	0.3952 (11)	0.0261 (15)	0.417 (5)
C11B	-0.001 (3)	0.4119 (9)	0.3461 (13)	0.0430 (17)	0.417 (5)
H11B	-0.1300	0.3819	0.3890	0.052*	0.417 (5)
C12B	0.060 (3)	0.3922 (7)	0.2342 (14)	0.049 (2)	0.417 (5)
H12B	-0.0276	0.3487	0.2007	0.059*	0.417 (5)
C13B	0.249 (3)	0.4360 (9)	0.1715 (11)	0.050(2)	0.417 (5)
H13B	0.2906	0.4225	0.0950	0.060*	0.417 (5)
C14B	0.377 (3)	0.4997 (8)	0.2206 (13)	0.051 (2)	0.417 (5)
H14B	0.5065	0.5297	0.1777	0.061*	0.417 (5)
C15B	0.316 (3)	0.5194 (8)	0.3324 (14)	0.0347 (17)	0.417 (5)
H15B	0.4041	0.5629	0.3660	0.042*	0.417 (5)
C16	-0.1906 (5)	0.71396 (17)	0.4340 (2)	0.0295 (6)	
H16	-0.1542	0.7504	0.4921	0.035*	
C17	-0.3839(5)	0.73363 (15)	0.3379 (2)	0.0277 (5)	
C18	-0.4040 (6)	0.68891 (15)	0.2402 (2)	0.0319 (6)	
H18	-0.2870	0.6449	0.2344	0.038*	
C19	-0.5926 (6)	0.70787 (19)	0.1514 (2)	0.0339 (6)	
H19	-0.6052	0.6778	0.0841	0.041*	
C20	-0.7634 (6)	0.77200 (16)	0.1630 (2)	0.0309 (6)	
C21	-0.7499 (6)	0.81762 (16)	0.2582 (2)	0.0310 (6)	
H21	-0.8692	0.8612	0.2637	0.037*	
C22	-0.5568 (6)	0.79807 (16)	0.3461 (2)	0.0316 (6)	
H22	-0.5423	0.8289	0.4124	0.038*	

Atomic displacement parameters  $(Å^2)$ 

	$U^{11}$	U <sup>22</sup>	U <sup>33</sup>	$U^{12}$	$U^{13}$	<i>U</i> <sup>23</sup>
S1	0.0408 (3)	0.0258 (3)	0.0297 (3)	0.0003 (3)	-0.0032 (2)	-0.0018 (3)
01A	0.045 (6)	0.033 (4)	0.0448 (18)	-0.007(5)	0.011 (5)	0.004 (2)

# supporting information

O1B	0.045 (6)	0.033 (4)	0.0448 (18)	-0.007 (5)	0.011 (5)	0.004 (2)
O2	0.0743 (17)	0.0657 (18)	0.0406 (12)	0.0136 (14)	-0.0202 (11)	-0.0143 (12)
03	0.0636 (15)	0.0471 (14)	0.0538 (14)	0.0174 (12)	-0.0183 (12)	0.0023 (11)
N1	0.0326 (11)	0.0294 (12)	0.0260 (11)	-0.0036 (10)	0.0002 (8)	0.0008 (9)
N2	0.0416 (13)	0.0419 (15)	0.0318 (12)	-0.0038 (12)	-0.0050 (10)	0.0034 (11)
C1	0.0416 (16)	0.0271 (15)	0.0328 (14)	-0.0008 (13)	0.0061 (12)	0.0022 (12)
C2	0.0332 (13)	0.0263 (14)	0.0248 (12)	-0.0002 (10)	0.0061 (10)	0.0016 (10)
C3	0.0331 (13)	0.0318 (15)	0.0262 (12)	0.0040 (11)	0.0050 (10)	0.0013 (11)
C4A	0.047 (4)	0.035 (4)	0.036 (3)	0.009 (3)	0.002 (2)	0.004 (2)
C5A	0.044 (3)	0.052 (3)	0.034 (3)	0.013 (2)	-0.0027 (18)	0.005 (2)
C6A	0.040 (3)	0.054 (3)	0.034 (2)	0.005 (3)	-0.005 (2)	0.002 (2)
C7A	0.035 (4)	0.041 (4)	0.028 (3)	0.006 (3)	0.000 (2)	-0.007 (4)
C4B	0.047 (4)	0.035 (4)	0.036 (3)	0.009 (3)	0.002 (2)	0.004 (2)
C5B	0.044 (3)	0.052 (3)	0.034 (3)	0.013 (2)	-0.0027 (18)	0.005 (2)
C6B	0.040 (3)	0.054 (3)	0.034 (2)	0.005 (3)	-0.005 (2)	0.002 (2)
C7B	0.035 (4)	0.041 (4)	0.028 (3)	0.006 (3)	0.000 (2)	-0.007 (4)
C8	0.0310 (13)	0.0346 (16)	0.0274 (13)	0.0042 (11)	0.0025 (10)	0.0014 (11)
C9	0.0313 (13)	0.0247 (14)	0.0270 (13)	-0.0019 (10)	0.0035 (10)	-0.0015 (10)
C10A	0.021 (4)	0.025 (2)	0.0314 (16)	0.006 (3)	-0.008 (2)	0.0031 (15)
C11A	0.046 (4)	0.034 (3)	0.048 (2)	-0.008 (3)	0.000 (3)	-0.0066 (18)
C12A	0.057 (5)	0.040 (3)	0.050 (3)	-0.005 (3)	-0.010 (3)	-0.014 (2)
C13A	0.066 (5)	0.051 (4)	0.035 (2)	0.001 (4)	0.001 (3)	-0.016 (2)
C14A	0.065 (5)	0.047 (3)	0.041 (3)	-0.014 (4)	0.016 (3)	-0.011 (2)
C15A	0.036 (5)	0.033 (2)	0.036 (2)	-0.006 (3)	0.001 (3)	-0.0046 (18)
C10B	0.021 (4)	0.025 (2)	0.0314 (16)	0.006 (3)	-0.008 (2)	0.0031 (15)
C11B	0.046 (4)	0.034 (3)	0.048 (2)	-0.008 (3)	0.000 (3)	-0.0066 (18)
C12B	0.057 (5)	0.040 (3)	0.050 (3)	-0.005 (3)	-0.010 (3)	-0.014 (2)
C13B	0.066 (5)	0.051 (4)	0.035 (2)	0.001 (4)	0.001 (3)	-0.016 (2)
C14B	0.065 (5)	0.047 (3)	0.041 (3)	-0.014 (4)	0.016 (3)	-0.011 (2)
C15B	0.036 (5)	0.033 (2)	0.036 (2)	-0.006 (3)	0.001 (3)	-0.0046 (18)
C16	0.0319 (12)	0.0288 (15)	0.0279 (11)	-0.0029 (11)	0.0007 (9)	-0.0002 (11)
C17	0.0279 (12)	0.0257 (13)	0.0295 (12)	-0.0045 (10)	0.0009 (10)	0.0043 (10)
C18	0.0368 (13)	0.0284 (16)	0.0308 (13)	0.0034 (11)	0.0061 (10)	-0.0007 (10)
C19	0.0421 (14)	0.0324 (14)	0.0270 (11)	0.0005 (14)	0.0011 (10)	-0.0064 (13)
C20	0.0313 (13)	0.0319 (15)	0.0296 (12)	-0.0043 (11)	-0.0004 (10)	0.0039 (11)
C21	0.0332 (13)	0.0268 (13)	0.0330 (14)	-0.0008 (11)	0.0002 (10)	0.0016 (11)
C22	0.0375 (14)	0.0282 (14)	0.0292 (12)	-0.0039 (11)	-0.0001 (10)	-0.0031 (11)

Geometric parameters (Å, °)

S1—C8	1.730 (3)	С7В—Н7ВА	0.9902	
S1—C9	1.758 (3)	C7B—H7BB	0.9900	
01A—C1	1.213 (18)	C7B—C8	1.55 (4)	
01B—C1	1.27 (3)	C10A—C11A	1.3900	
O2—N2	1.214 (4)	C10A—C15A	1.3900	
O3—N2	1.221 (4)	C11A—H11A	0.9500	
N1—C9	1.384 (3)	C11A—C12A	1.3900	
N1-C16	1.282 (4)	C12A—H12A	0.9500	

N2-C20	1.470 (3)	C12A—C13A	1.3900
C1—C2	1.487 (4)	C13A—H13A	0.9500
C1C10A	1.499 (9)	C13A—C14A	1.3900
C1—C10B	1.493 (13)	C14A—H14A	0.9500
C2—C3	1.437 (4)	C14A—C15A	1.3900
C2—C9	1.378 (4)	C15A—H15A	0.9500
C3—C4A	1.51 (3)	C10B—C11B	1.3900
C3—C4B	1.50 (4)	C10B—C15B	1.3900
C3—C8	1.359 (4)	C11B—H11B	0.9500
C4A—H4AA	0.9898	C11B—C12B	1.3900
C4A—H4AB	0.9899	C12B—H12B	0.9500
C4A - C5A	1 537 (14)	C12B— $C13B$	1 3900
C5A—H5AA	0.9902	C13B—H13B	0.9500
C5A—H5AB	0.9899	C13B— $C14B$	1 3900
C5A - C6A	1 523 (9)	C14B—H14B	0.9500
C6A - H6AA	0.9900	C14B— $C15B$	1 3900
C6A—H6AB	0.9900	C15B—H15B	0.9500
C6A - C7A	1.550(13)	C16—H16	0.9500
C7A - H7AA	0.9900	C16-C17	1.462(3)
C7A - H7AB	0.9900	C17 - C18	1.402(3) 1.303(4)
C7A-C8	1.48(2)	C17 - C13	1.395 (4)
CAB HABA	0.9900	C18—H18	0.9500
C4B—H4BB	0.9901	C18 - C19	1.382(4)
C4B C5B	1.524(17)	$C_{10} = C_{19}$	0.9500
$C_{1}^{-}$	0.0000	C19 $C20$	1.380(4)
C5B H5BB	0.9900	$C_{19} = C_{20}$	1.339(4) 1.377(4)
C5P C6P	0.9899	$C_{20} = C_{21}$	0.9500
	1.311(12)	$C_{21}$ $C_{21}$ $C_{22}$	0.9300
	0.9900	$C_{21}$ $C_{22}$ $C$	1.390 (4)
COD-RODD	0.9900 1 552 (17)	C22—H22	0.9300
COD-C/D	1.335 (17)		
C8—S1—C9	91.40 (14)	C8—C7B—H7BB	113.4
C16—N1—C9	119.2 (2)	C3—C8—S1	112.3 (2)
02—N2—O3	123.5 (3)	C3—C8—C7A	123.4 (5)
O2—N2—C20	118.4 (3)	C3—C8—C7B	130.5 (6)
O3—N2—C20	118.1 (2)	C7A—C8—S1	124.3 (5)
01A-C1-C2	118.8 (9)	C7B—C8—S1	117.1 (6)
01A-C1-C10A	117.4 (10)	N1—C9—S1	123.3(2)
O1B-C1-C2	117.5 (13)	C2—C9—S1	110.8 (2)
01B-C1-C10B	118.0 (15)	C2—C9—N1	125.8 (2)
C2-C1-C10A	121.2 (5)	C11A—C10A—C1	116.5 (7)
C2-C1-C10B	122.5(7)	C11A— $C10A$ — $C15A$	120.0
$C_3 - C_2 - C_1$	122.2(2)	C15A— $C10A$ — $C1$	123.5 (7)
C9—C2—C1	125.0 (2)	C10A—C11A—H11A	120.0
C9—C2—C3	112.6 (2)	C12A— $C11A$ — $C10A$	120.0
C2-C3-C4A	122.6 (5)	C12A— $C11A$ — $H11A$	120.0
C2-C3-C4B	130.1 (8)	C11A - C12A - H12A	120.0
C8-C3-C2	112.9 (2)	C11A - C12A - C13A	120.0

C8—C3—C4A	124.5 (5)	C13A—C12A—H12A	120.0
C8—C3—C4B	117.0 (8)	C12A—C13A—H13A	120.0
С3—С4А—Н4АА	110.8	C14A—C13A—C12A	120.0
С3—С4А—Н4АВ	108.5	C14A—C13A—H13A	120.0
C3—C4A—C5A	109.3 (14)	C13A—C14A—H14A	120.0
H4AA—C4A—H4AB	108.6	C15A—C14A—C13A	120.0
С5А—С4А—Н4АА	110.8	C15A—C14A—H14A	120.0
C5A—C4A—H4AB	108.7	C10A—C15A—H15A	120.0
С4А—С5А—Н5АА	110.6	C14A—C15A—C10A	120.0
С4А—С5А—Н5АВ	107.8	C14A—C15A—H15A	120.0
Н5АА—С5А—Н5АВ	107.9	C11B—C10B—C1	119.7 (11)
C6A—C5A—C4A	111.7 (11)	C11B—C10B—C15B	120.0
С6А—С5А—Н5АА	109.7	C15B—C10B—C1	119.6 (10)
С6А—С5А—Н5АВ	109.0	C10B—C11B—H11B	120.0
С5А—С6А—Н6АА	109.7	C12B—C11B—C10B	120.0
С5А—С6А—Н6АВ	109.7	C12B—C11B—H11B	120.0
C5A—C6A—C7A	109.1 (9)	C11B—C12B—H12B	120.0
Н6АА—С6А—Н6АВ	108.3	C13B—C12B—C11B	120.0
С7А—С6А—Н6АА	111.8	C13B—C12B—H12B	120.0
С7А—С6А—Н6АВ	108.2	C12B—C13B—H13B	120.0
C6A—C7A—H7AA	107.9	C14B—C13B—C12B	120.0
С6А—С7А—Н7АВ	110.4	C14B—C13B—H13B	120.0
Н7АА—С7А—Н7АВ	107.5	C13B—C14B—H14B	120.0
C8—C7A—C6A	110.0 (13)	C13B—C14B—C15B	120.0
С8—С7А—Н7АА	109.1	C15B—C14B—H14B	120.0
С8—С7А—Н7АВ	111.9	C10B—C15B—H15B	120.0
C3—C4B—H4BA	106.4	C14B—C15B—C10B	120.0
C3—C4B—H4BB	111.5	C14B—C15B—H15B	120.0
C3—C4B—C5B	113 (2)	N1—C16—H16	119.0
H4BA—C4B—H4BB	107.7	N1—C16—C17	122.0 (3)
C5B—C4B—H4BA	106.4	C17—C16—H16	119.0
C5B—C4B—H4BB	111.0	C18—C17—C16	121.7 (2)
C4B—C5B—H5BA	107.1	C18—C17—C22	119.5 (2)
C4B—C5B—H5BB	110.3	C22—C17—C16	118.8 (2)
H5BA—C5B—H5BB	108.2	C17—C18—H18	119.7
C6B—C5B—C4B	112.0 (16)	C19—C18—C17	120.6 (3)
C6B—C5B—H5BA	110.4	C19—C18—H18	119.7
C6B—C5B—H5BB	108.8	C18—C19—H19	120.9
С5В—С6В—Н6ВА	108.9	C18—C19—C20	118.3 (2)
C5B—C6B—H6BB	109.6	С20—С19—Н19	120.9
C5B—C6B—C7B	111.6 (15)	C19—C20—N2	118.6 (2)
H6BA—C6B—H6BB	107.7	C21—C20—N2	118.6 (3)
С7В—С6В—Н6ВА	106.1	C21—C20—C19	122.8 (2)
С7В—С6В—Н6ВВ	112.8	C20—C21—H21	121.0
С6В—С7В—Н7ВА	107.1	C20—C21—C22	118.1 (3)
C6B—C7B—H7BB	113.8	C22—C21—H21	121.0
H7BA—C7B—H7BB	108.2	C17—C22—H22	119.6
C8—C7B—C6B	106.3 (17)	C21—C22—C17	120.7 (3)
			(0)

С8—С7В—Н7ВА	107.7	C21—C22—H22	119.6
O1A—C1—C2—C3	40.0 (6)	C4B—C3—C8—S1	-178.4 (18)
O1A—C1—C2—C9	-133.7 (5)	C4B—C3—C8—C7A	4 (2)
O1A-C1-C10A-C11A	25.5 (8)	C4B—C3—C8—C7B	-3 (2)
O1A—C1—C10A—C15A	-155.8 (7)	C4B—C5B—C6B—C7B	63 (2)
O1A-C1-C10B-C11B	14.0 (11)	C5B—C6B—C7B—C8	-43 (2)
O1A—C1—C10B—C15B	-157.1 (8)	C6B—C7B—C8—S1	-169.6 (11)
O1B—C1—C2—C3	60.5 (10)	C6B—C7B—C8—C3	16 (3)
O1B—C1—C2—C9	-113.2 (10)	C6B—C7B—C8—C7A	-25(10)
O1B-C1-C10A-C11A	5.2 (11)	C8—S1—C9—N1	174.9 (2)
O1B-C1-C10A-C15A	-176.1(10)	C8—S1—C9—C2	-0.8(2)
O1B-C1-C10B-C11B	-6.6(13)	C8-C3-C4A-C5A	-16(2)
O1B $C1$ $C10B$ $C15B$	-1777(11)	C8-C3-C4B-C5B	10(2)
02 - N2 - C20 - C19	11(4)	C9 - S1 - C8 - C3	-11(2)
02 - N2 - C20 - C21	-1793(3)	C9 - S1 - C8 - C7A	1767(11)
02 N2 C20 C21	179.9 (3)	C9 = S1 = C8 = C7B	-176.8(14)
03 - N2 - C20 - C21	-0.5(4)	C9 - N1 - C16 - C17	-179.2(2)
N1 - C16 - C17 - C18	-123(4)	C9-C2-C3-C4A	175.2(2)
N1 C16 C17 C22	12.3 (4)	$C_{1}^{0} = C_{2}^{0} = C_{3}^{0} = C_{4}^{0} R$	173.7(13) 178(2)
$N_{1} = C_{10} = C_{17} = C_{22}$ $N_{2} = C_{20} = C_{21} = C_{22}$	-179.6(2)	$C_{2} - C_{2} - C_{3} - C_{4}$	-32(3)
$C_1 - C_2 - C_3 - C_4 \Delta$	179.0(2) 1 3 (14)	$C_{10} = C_{2} = C_{3} = C_{3}$	-1212(3)
C1 - C2 - C3 - C4B	4(2)	C10A - C1 - C2 - C3	121.2(4)
$C_1 = C_2 = C_3 = C_4 D$	-177.6(3)	$C_{10A} = C_1 = C_2 = C_3$	102(5)
$C_1 - C_2 - C_3 - C_3$	177.0(3)	C10A - C1 - C10B - C15B	-69(5)
C1 - C2 - C9 - N1	1/0.5(2) 1.0(4)	C10A - C11A - C12A - C13A	0.0
C1 - C10A - C11A - C12A	1.0 (4)	C11A - C10A - C15A - C14A	0.0
C1 = C10A = C15A = C12A	-1787(0)	$C_{11A} = C_{10A} = C_{13A} = C_{14A}$	0.0
C1 = C10R = C11R = C12R	-171.1(11)	C12A C13A C14A C15A	0.0
C1 = C10B = C15B = C14B	171.1(11) 171.1(11)	C12A = C13A = C14A = C15A	0.0
$C_1 = C_1 O_2 = C_1 O_2 = C_1 O_2 O_2 O_2 O_2 O_2 O_2 O_2 O_2 O_2 O_2$	-173 1 (3)	C15A = C14A = C15A = C10A	0.0
$C_2 = C_1 = C_{10A} = C_{11A}$	5 6 (7)	C10R C1 C2 C3	-135.7(7)
$C_2 = C_1 = C_{10}R = C_{11}R$	-170.3(5)	C10B - C1 - C2 - C3	133.7(7)
$C_2 = C_1 = C_{10B} = C_{11B}$	170.3(5) 18.6(11)	C10B = C1 = C2 = C3	-73(5)
$C_2 = C_1 = C_{10} = C_{13} = C_{10}$	16.0(11)	C10B - C1 - C10A - C11A	105 (5)
$C_2 = C_3 = C_4 A = C_5 B$	-162 1 (11)	C10B - C1 - C10A - C13A	105(5)
$C_2 = C_3 = C_4 = C_5 $	102.1(11)	C10B - C10B - C12B - C13B	0.0
$C_2 = C_3 = C_6 = S_1$	2.0(3)	$C_{11B} = C_{10B} = C_{13B} = C_{14B}$	0.0
$C_2 = C_3 = C_6 = C_7 R$	-173.2(11)	C12B - C12B - C13B - C14B	0.0
$C_2 - C_3 - C_6 - C_7 B$	1/7.0(17) 2.2(2)	C12B - C13B - C14B - C13B	0.0
$C_{3} = C_{2} = C_{3} = S_{1}$	2.3(3) -172 2(2)	C15D - C14D - C15D - C10D	0.0
$C_3 = C_2 = C_9 = N_1$	-1/5.5(2)	$C16 \qquad N1 \qquad C0 \qquad S1$	-14.8(4)
$C_3 = C_4 A = C_5 A = C_6 A$	43.3(19) -40(2)	$C_{10} = N_1 = C_9 = S_1$	-14.0(4)
$C_{4} = C_{4} = C_{5} = C_{6} = C_{6$	-148(21)	$C_{10} = N_1 = C_2 = C_2$	100.3(3)
$C_{4A} = C_{2} = C_{4B} = C_{3B}$	-140(21) -1762(12)	$C_{10} - C_{17} - C_{10} - C_{19}$	1/0.7(2) -1791(2)
$C_{4A} = C_{2} = C_{0} = C_{1A}$	-1/0.3(13)	$C_{10} - C_{17} - C_{22} - C_{21}$	-1/6.1(2)
$C_{A} = C_{A} = C_{A$	-1(2)	C17 - C10 - C19 - C20 C18 - C17 - C22 - C21	-0.8(4)
$C_{AA} = C_{5A} = C_{6A} = C_{7A}$	-1(2)	$C_{10} - C_{1} - C_{22} - C_{21}$	0.3(4)
U4A-UJA-U0A-U/A	-03.1 (10)	U10-U19-U20-IN2	-1/9./(2)

C5A—C6A—C7A—C8 C6A—C7A—C8—S1	51.0 (15) 159.4 (6)	C18—C19—C20—C21 C19—C20—C21—C22	0.8 (4) -0.1 (4)
C6A—C7A—C8—C3	-23.0 (18)	C20-C21-C22-C17	-0.6(4)
C6A—C7A—C8—C7B	120 (13)	C22-C17-C18-C19	0.2 (4)
C4B—C3—C4A—C5A	-2 (18)		

Hydrogen-bond geometry (Å, °)

D—H···A	D—H	H···A	D··· $A$	D—H···A
$\overline{\text{C4}A-\text{H4}AA\cdots\text{O1}B^{\text{i}}}$	0.99	2.38	3.15 (4)	135
C4 $B$ —H4 $BA$ ···O1 $A^{i}$	0.99	2.50	3.45 (4)	162
C4 $B$ —H4 $BA$ ···O1 $B^{i}$	0.99	2.26	3.18 (4)	154
C7 <i>B</i> —H7 <i>BB</i> ···O2 <sup>ii</sup>	0.99	2.46	3.44 (3)	169
C13 <i>B</i> —H13 <i>B</i> ···O3 <sup>iii</sup>	0.95	2.55	3.371 (13)	145
C21—H21···O1 $A^{iv}$	0.95	2.40	3.127 (18)	133
C21—H21···O1 $B^{iv}$	0.95	2.44	3.13 (3)	129

Symmetry codes: (i) *x*+1, *y*, *z*; (ii) *x*+1, *y*, *z*+1; (iii) -*x*-1, *y*-1/2, -*z*; (iv) -*x*-1, *y*+1/2, -*z*+1.